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Multiphysics system analysis and optimization under uncertainty

Mathieu Balesdent, Loïc Brevault mathieu.balesdent@onera.fr

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Example of multiphysics system (launcher)



Complex process, numerous disciplines / physics



Presence of uncertainty at all the design phases

Early design of multiphysics aerospace systems



- Need to explore large number of candidate architectures at reasonable computational cost
- Need to master uncertainties relative to breakthrough technology models and environmental conditions to compare the solutions and assess trade-off



Outline

Multiphysics / Multidisciplinary system Design Analysis and Optimization Mathematical modeling Coupled and decoupled approaches Single-level and multi-level formulations

2 Multiphysics system design in uncertainty Problem formulation Overview of several approaches for multiphysics system optimization under uncertainties



4 Hot topics

5 Concluding remarks



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Multiphysics / Multidisciplinary system Design Analysis and Optimization Mathematical modeling Coupled and decoupled approaches Single-level and multi-level formulations

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3 Illustration on aerospace vehicle design

4 Hot topics

5 Concluding remarks



Modeling of multiphysics system





Modeling of multiphysics system





Classical approach vs MDAO

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Mathematical modeling of coupled multiphysics problem



- z : design variables
- y : input coupling variables
- c : output coupling functions







Mathematical modeling of coupled multiphysics problem



- z : design variables
- y : input coupling variables
- c : output coupling functions

System of non linear equations









[Balesdent et al., 2012, Martins and Lambe, 2013]







- c : coupling functions
- f : objective function
- g : inequality constraints

[Balesdent et al., 2012, Martins and Lambe, 2013]





















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Coupled and decoupled formulations



Couplings

 Interdisciplinary couplings satisfied at each iteration of the optimization process by an auxiliary solver (Gauss-Seidel, Newton, etc.)





Coupled and decoupled formulations







Coupled and decoupled formulations [Cramer et al., 1994]

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Coupled and decoupled formulations



Couplings

 Interdisciplinary couplings satisfied at each iteration of the optimization process by an auxiliary solver (MultiDisciplinary Analysis - MDA)



Couplings

- Couplings variables handled by the optimization process
- Equality constraints satisfied at the convergence of the optimization





Single-level vs Multilevel formulations







Single-level vs Multilevel formulations







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For multidisciplinary system analysis and optimization, individual discipline uncertainties are combined making the system analysis and optimization more complex [Brevault et al., 2020].

Three nested loops :

- multidisciplinary analysis,
- uncertainty propagation,
- optimization.







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Three nested loops :

- multidisciplinary analysis,
- uncertainty propagation,
- optimization.

Need for methods to handle the numerical cost involved by these loops













Coupling solving for system under uncertainty









- y : coupling variables
- z : design variables
- c : coupling functions
- f : objective function
- g : inequality constraints

U : uncertain variables





- MDA	40
min wrt st	y, z

UMDAO min wrt Θ[Y], z st

- y : coupling variables
- z : design variables
- c : coupling functions
- f : objective function
- g : inequality constraints

- U : uncertain variables
- $\Theta[Y]$: coupling variables





 MDA	.O —	
min wrt st	f(y, z) y, z	

- y : coupling variables
- z : design variables
- c : coupling functions
- f : objective function
- g : inequality constraints

_	UMDAO		
	min wrt st	Ξ[f(Θ[Y], z, U)] Θ[Y], z	

- U : uncertain variables
- $\Theta[\mathbf{Y}]$: coupling variables
- $\Xi[\cdot]$: measure of uncertainty on the objective function
- worst-case : $\min_{\Theta[\mathbf{Y}], z} \max_{\mathbf{U}} f(\Theta[\mathbf{Y}], z, \mathbf{U})$
- reliability-based formulation : $\mathbb{P}(\mathbf{g}(\boldsymbol{\Theta}[\mathbf{Y}], \mathbf{z}, \mathbf{U}) \leq 0)$



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C MD	AO	
min wrt st	$\begin{array}{c} f(\textbf{y},\textbf{z})\\ \textbf{y},\textbf{z}\\ \textbf{g}(\textbf{y},\textbf{z}) \leq 0 \end{array}$	

- y : coupling variables
- z : design variables
- c : coupling functions
- f : objective function
- g : inequality constraints

min	$\Xi[f(\Theta[\mathbf{Y}], \mathbf{z}, \mathbf{U})]$	
wrt	Θ[Y], z	
st	$K_{g}[g(\Theta[Y], z, U)] \leq 0$	

- U : uncertain variables
- $\Xi[\cdot]$: measure of uncertainty on the objective function
- K.[·] : measure of constraint satisfaction under uncertainty







$$\begin{array}{|c|c|c|c|} \hline \mathsf{MDAO} & & \\ \hline min & \mathbf{f}(\mathbf{y}, \mathbf{z}) \\ wrt & \mathbf{y}, \mathbf{z} \\ st & \mathbf{g}(\mathbf{y}, \mathbf{z}) \leq 0 \\ \forall j \neq i, \mathbf{y}_{ji} = \mathbf{c}_{ji}(\mathbf{y}_{\cdot j}, \mathbf{z}_{j}) \end{array}$$

- y : coupling variables
- z : design variables
- c : coupling functions
- f : objective function
- g : inequality constraints

 $\begin{array}{c|c} & \mathsf{UMDAO} \\ & \min & \Xi[f(\Theta[\mathbf{Y}], \mathbf{z}, \mathbf{U})] \\ & \mathsf{wrt} & \Theta[\mathbf{Y}], \mathbf{z} \\ & \mathsf{st} & \mathsf{K}_{g}[\mathbf{g}(\Theta[\mathbf{Y}], \mathbf{z}, \mathbf{U})] \leq 0 \\ & \forall j \neq i, \mathsf{K}_{y}[\mathbf{Y}_{ji}(\Theta[\mathbf{Y}]) = \mathbf{c}_{ji}(\Theta[\mathbf{Y}_{\cdot j}], \mathbf{z}_{j}, \mathbf{U})] \leq 0 \end{array}$

- U : uncertain variables
- Ξ[·] : measure of uncertainty on the objective function [Lelièvre et al., 2016]
- K.[·] : measure of constraint satisfaction under uncertainty







MDAO vs UMDAO



- y : coupling variables
- z : design variables
- c : coupling functions
- **f** : objective function
- g : inequality constraints

— UMDAO	
min wrt st ∀j ≠	$ \begin{split} &\Xi[f(\Theta[\mathbf{Y}],\mathbf{z},U)]\\ &\Theta[\mathbf{Y}],\mathbf{z}\\ &\kappa_{g}[\mathbf{g}(\Theta[\mathbf{Y}],\mathbf{z},U)] \leq 0\\ &i,\kappa_{y}[\mathbf{Y}_{ji}(\Theta[\mathbf{Y}]) = \mathbf{c}_{ji}(\Theta[\mathbf{Y}_{\cdot j}],\mathbf{z}_{j},U)] \leq 0 \end{split} $

Key point : Which measure to take for the coupling satisfaction under uncertainties?

- $\rightarrow \forall j \neq i, \, \mathsf{K}_{\mathsf{y}}[\mathsf{Y}_{ji}(\boldsymbol{\Theta}[\mathsf{Y}]) = \mathsf{c}_{ji}(\boldsymbol{\Theta}[\mathsf{Y}_{\cdot j}], \mathsf{z}_{j}, \mathsf{U})] \leq 0$
 - · distribution or statistical moments,
 - at a specific realization,
 - for all the realizations.





MultiDiscipline Feasible with uncertainty

min $\Xi[f(\mathbf{z}, \mathbf{Y}(\mathbf{z}, \mathbf{U}), \mathbf{U})]$

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w.r.t. s.t.

- $\mathbb{K}_k[g_k(\mathsf{z},\mathsf{Y}(\mathsf{z},\mathsf{U}),\mathsf{U})] \leq 0 \ \forall k$
- Most basic optimization framework
- Excessively expensive : three embedded loops : MDA inside UQ inside optimization [Haldar and Mahadevan, 2000, Jaeger et al., 2013]







• Full MDA at the mean value of the uncertainties μ_{U} to get $\mu_{Y_{ij}}$.







- Full MDA at the mean value of the uncertainties μ_U to get μ_{Y_{ij}}.
- 2 Approximate the coupling variables by their first order Taylor expansion [Du and Chen, 2002] :

$$\begin{split} \hat{\mathbf{Y}}_{ij}\left(\mathbf{z},\mathbf{Y}_{.i},\mathbf{u}_{i}\right) &= \left. \left. \boldsymbol{\mu}_{\mathbf{Y}_{ij}} + \frac{\partial \mathbf{c}_{ij}}{\partial \mathbf{u}_{i}} \right|_{\mathbf{u}=\boldsymbol{\mu}_{\mathbf{u}}} \left(\mathbf{u}_{i} - \boldsymbol{\mu}_{\mathbf{u}_{i}}\right) \\ &+ \frac{\partial \mathbf{c}_{ij}}{\partial \mathbf{Y}_{.i}} \bigg|_{\mathbf{u}=\boldsymbol{\mu}_{\mathbf{u}}} \left(\mathbf{Y}_{.i} - \boldsymbol{\mu}_{\mathbf{Y}_{.i}}\right) \end{split}$$







- Full MDA at the mean value of the uncertainties μ_U to get μ_{Y_{ij}}.
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8 Replace MDA by the linearized system of equations :

$$\mathbf{\hat{Y}}(\mathbf{u}) = \mathbf{A}^{-1}\mathbf{B}(\mathbf{U} - \boldsymbol{\mu}_{\mathbf{U}})$$







Replace MDA by the linearized system of equations :

$$\mathbf{\hat{Y}}(\mathbf{u}) = \mathbf{A}^{-1}\mathbf{B}(\mathbf{U} - \boldsymbol{\mu}_{\mathbf{U}})$$

In case robust problem formulation is used $\Xi[\cdot] = \mathbb{E}[\cdot] + k\sigma[\cdot]$, mean value and variance of output measure can be also derived analytically model using hypothesis of linearity and independent (Normal) uncertainty. [Du and Chen, 2002]






Concurrent SubSystem Uncertainty Analysis - Illustration

Let consider the following two discipline system [Brevault et al., 2020] :

$$\begin{array}{rcl} - \mbox{ Discipline 1 : } y_{12} & = & -z_{sh}^{0.2} + u_{sh} + 0.25 \times u_1^{0.2} + z_1 + y_{21}^{0.58} + u_1^{0.4} \times y_{21}^{0.47} \\ - \mbox{ Discipline 2 : } y_{21} & = & -z_{sh} + u_{sh}^{0.1} - z_2^{0.1} + 3 \times y_{12}^{0.47} + u_2^{0.33} \\ & & + y_{12}^{0.26} \times u_2^{0.05} + y_{12}^{0.6} \times u_2^{0.13} + 100 \end{array}$$





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and the objective and constraint functions :

Objective :
$$f = \left(\frac{1}{5}\right) \times \left[(z_{sh} - 4)^2 + (z_1 - 3)^2 + (z_2 - 2)^2 + (y_{21} + z_1 \times z_2)^{0.6} + (u_{sh} + 0.9)^2\right]$$

Constraint : $g = \exp(-0.01 \times u_1^2) \times (z_{sh} - 1) \times z_1 - 0.02 \times u_2^5 \times z_2^3 + 0.01 \times y_{12}^{2.5} \times z_2 \times \exp(-0.1 \times u_{sh})$





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and the objective and constraint functions :

Objective : $f = \left(\frac{1}{5}\right) \times \left[(z_{sh} - 4)^2 + (z_1 - 3)^2 + (z_2 - 2)^2 + (y_{21} + z_1 \times z_2)^{0.6} + (u_{sh} + 0.9)^2\right]$ Constraint : $g = \exp(-0.01 \times u_1^2) \times (z_{sh} - 1) \times z_1 - 0.02 \times u_2^5 \times z_2^3 + 0.01 \times y_{12}^{2.5} \times z_2 \times \exp(-0.1 \times u_{sh})$ • $U_{sh} \sim \mathcal{N}(2, 0.3)$ Reference solution obtained by MDF with CMC :

- $\mathbf{z} = [0.6; 0.2; 0.0]^T$
- Objective function : 7.95



• $U_1 \sim \mathcal{N}(0.5, 0.1)$

• $U_2 \sim \mathcal{N}(4, 0.5)$



Concurrent SubSystem Uncertainty Analysis - Illustration







Concurrent SubSystem Uncertainty Analysis - Illustration

Convergence to the same design point as MDF with a reduction factor of 10^3 : $N_{opt} \times N_{MDA} \times N_{CMC} \rightarrow N_{opt}$



in case
$$U_1 \sim \mathcal{U}(0, 1)$$

But method strongly limited to quasi-linear problems with independent (Normal) uncertainty distributions.





Sequential Optimization and Reliability Analysis [Du et al., 2008]









Sequential Optimization and Reliability Analysis [Du et al., 2008]





I	Search for most probable point (inverse FORM)				
	max	h(u)			
	wrt	и, у			
	st	$\mathbf{g}(\mathbf{z_{opt}},\mathbf{y},\mathbf{u})=0$			
		$\forall i \neq j, \; \mathbf{y}_{ij} = \mathbf{c}_{ij}(\mathbf{z_{opt}}, \mathbf{y}_{.i}, \mathbf{u}_i)$			





Sequential Optimization and Reliability Analysis [Du et al., 2008]



- Solving of deterministic MDO problem with uncertain variables fixed at the MPP u*,
- Search of MPP (e.g. FORM) : design variables are fixed at their current optimal values z_{opt}, coupling constraints are imposed
- Generic approach that can be applied to all MDO formulations, either coupled or decoupled [Li et al., 2010, Li et al., 2014, Ahn and Kwon, 2006]





Sequential Optimization and Reliability Analysis

Comparison with MDF. Same function as before but :

- $U_{sh} \sim \mathcal{N}(2, 0.3)$
- $U_1 \sim \mathcal{U}(0, 1.)$
- $U_2 \sim \mathcal{N}(4, 0.5)$



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Statistical moment matching [Liu et al., 2006]

- Coupling variables handled by the optimizer : *q* first statistical moments of coupling variables : Θ[Y] = {M₁[Y], ..., M_q[Y]} with hypothesis on their distributions.
- Allow "deterministic handling" of coupling variables

Possible improvement : Let the optimizer handle all the covariance terms of coupling variables [Ghosh et al., 2014].





Same problem as before, use of multi-level matching moment methods, name matching moment collaborative optimization [Xiong et al., 2014]. Hypothesis of coupling variables are Normally distributed ...





Integral form of coupling satisfaction under uncertainties

For a coupling relationship y_{ij} between disciplines *i* and *j* :

Deterministic decoupled approach : -

• $y_{ij} = c_{ij}(z_i, y_i)$: one equality constraint





Integral form of coupling satisfaction under uncertainties

For a coupling relationship y_{ij} between disciplines *i* and *j* :

Deterministic decoupled approach : -

• $y_{ij} = c_{ij}(z_i, y_i)$: one equality constraint

Decoupled approach under uncertainties : -

• $\forall \mathbf{u} \in \Omega, \ y_{ij}(\mathbf{u}) = c_{ij}(z_i, y_{i}(\mathbf{u}), \mathbf{u}) : \infty \text{ of equality constraints}$

• Integral form :
$$\int_{\Omega} \left[y_{ij}(\mathbf{u}) - c_{ij}(\mathbf{z}_i, y_i(\mathbf{u}), \mathbf{u}) \right]^2 h_{\mathbf{U}}(\mathbf{u}) d\mathbf{u} = 0$$

- How let the optimizer handle $y_{ij}(\mathbf{u})$?
 - Use of surrogate model : Polynomial Chaos Expansion (PCE) $y_{ij}(\mathbf{u}) \rightarrow \hat{y}_{ij}(\mathbf{u}, \boldsymbol{\alpha})$
 - α : coefficients of PCE handled by the optimizer (\rightarrow new coupling variables).





IDF-PCE (Individual Discipline Feasible - Polynomial Chaos Expansion) [Brevault et al., 2016, Brevault et al., 2020, Liu et al., 2022]

- Iterative training of surrogate model of coupling relationships,
- Surrogate model : Polynomial Chaos Expansion (PCE),
- Optimizer handles design variables z and PCEs coefficients α,
- Surrogate models mimic, at the convergence of the optimization process, coupling relationship as MDA does.







Formulation IDF-PCE

$$\begin{array}{ll} \min & \Xi[f(\mathbf{z}, \boldsymbol{\alpha}, \mathbf{U})] & (1) \\ \text{wrt} & \mathbf{z}, \boldsymbol{\alpha} & (2) \\ \text{st} & \boldsymbol{K}[\mathbf{g}(\mathbf{z}, \boldsymbol{\alpha}, \mathbf{U})] \leq 0 & (3) \\ & \forall i \neq j, \ J_{(m_{ij})} = \int_{\Omega} \left[\mathbf{c}_{ij} \left(\mathbf{z}_{i}, \mathbf{u}_{i}, \hat{\mathbf{y}}_{.i} \left(\mathbf{u}, \boldsymbol{\alpha}^{(.i)} \right) \right) - \hat{\mathbf{y}}_{ij} \left(\mathbf{u}, \boldsymbol{\alpha}^{(ij)} \right) \right]_{(m_{ij})}^{2} h_{\mathbf{U}}(\mathbf{u}) d\mathbf{u} = 0 & (4) \end{array}$$

•
$$\hat{\mathbf{y}}_{.i}$$
 ($\mathbf{u}, \boldsymbol{\alpha}^{(.i)}$) PCEs of all coupling variables *i*,

• PCEs coefficients α handled at system level,

Three approaches to estimate integrals (Eq. (4)) :

- Monte-Carlo,
- Quadratures,
- Decomposition of output coupling variables over other PCEs.





IDF - PCE, illustration

Comparison with MDF. Same function as before but :

- $U_{sh} \sim \mathcal{U}(-1,1)$
- $U_1 \sim \mathcal{U}(0,1)$
- $U_2 \sim \mathcal{N}(0,1)$





Results

Results	MDF-MDA (ref)	IDF-PCE (MC)	IDF-PCE (quadrature)	IDF-PCE (PCE)
Objective	$\mu_{F} = 0.928$	$\mu_{F} = 0.926$	$\mu_{F} = 0.926$	$\mu_{F} = 0.914$
Design	$z_{sh} = 0.520$	$z_{sh} = 0.511$	$z_{sh} = 0.514$	$z_{sh} = 0.523$
variables	$z_1 = 0.340$	$z_1 = 0.339$	$z_1 = 0.340$	$z_1 = 0.349$
	$z_2 = 0.658$	$z_2 = 0.661$	$z_2 = 0.661$	$z_2 = 0.649$
Contraintes	$ c_{12} - y_{12} ^2 \le 0.0001$	$J_{12} = 0.00067$	$J_{12} = 0.00054$	$\ \boldsymbol{\alpha}^{(21)} - \tilde{\boldsymbol{\alpha}}^{(21)} \ ^2 = 0.48$
couplage	$\ c_{21} - y_{21}\ ^2 \le 0.0001$	$J_{21} = 0.00057$	$J_{21} = 0.00074$	$\ \boldsymbol{\alpha}^{(21)} - \tilde{\boldsymbol{\alpha}}^{(21)} \ ^2 = 0.3$
Nb iterations	$N_{i} = 2016$	$N_{i} = 5608$	$N_{i} = 5501$	$N_{i} = 5262$
of optimiza-				
tion				
Nb calls disci-	$N_{cl} = 1512 * 10^6$	$N_{cl} = 841.2 * 10^6$	$N_{cl} = 3.52 * 10^6$	$N_{cl} = 3.37 * 10^6$
plines	0	U	U	0
Speed-up fac-	1 (ref)	1.80	429.55	448.66
tor				





Results - distribution



Classification of approaches [Brevault et al., 2020]







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Application to space vehicle design



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- Minimization of the expected value of the Gross Lift Off Weight (GLOW)
- Constraints : reach GTO orbit
- Number of design variables : 27
- Number of uncertain variables : 3



Deterministic solution







Deterministic solution



Deterministic MDO \Rightarrow **Non robust to uncertainties**





Optimal solution with handling of uncertainties



[Balesdent et al., 2016, Brevault et al., 2020]





Optimal solution with handling of uncertainties



UMDO solution \Rightarrow improvement of robustness to uncertainties

[Balesdent et al., 2016, Brevault et al., 2020]





Optimal solution with handling of uncertainties



Speed up factor with respect to coupled approach : ~ 11

[Balesdent et al., 2016, Brevault et al., 2020]





Launch vehicle geometry and 3D trajectories









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 Decoupled/distributed sensitivity analysis



• How to use disciplinary SA results (*e.g.* Sobol indices) to provide information on global multiphysics SA?

[Liu et al., 2021]





- Decoupled/distributed sensitivity analysis
- Surrogate model in the multiphysics analysis





- Which surrogate model?
- How to define adaptive strategies to refine consistently with respect to the coupling satisfaction ? [Dubreuil et al., 2020]





- Decoupled/distributed sensitivity analysis
- Surrogate model in the multiphysics analysis
- Multi-fidelity modeling of multiphysics system



• Which physics / model to refine ? How ? At which level (*e.g.* MDA, disciplinary level ?)

> [Kontogiannis and Savill, 2020, Garland et al., 2020]





- Decoupled/distributed sensitivity analysis
- Surrogate model in the multiphysics analysis
- Multi-fidelity modeling of multiphysics system
- Field distributed coupling variable



 How to model field coupling variables and handle them in multiphysics optimization?

[Degroote, 2013, Berthelin et al., 2021]





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Concluding remarks

• UQ for multiphysics system analysis and design is a very dynamic field of research and applied in various domains (aerospace, civil engineering, automotive, structure, *etc.*),





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- Numerous methods allow now to perform design with uncertainties from modeling to optimization under uncertainties while accounting for multiphysics couplings,





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- Numerous methods allow now to perform design with uncertainties from modeling to optimization under uncertainties while accounting for multiphysics couplings,
- Several methodological breakthroughs are still locked and need further research (*e.g.* high dimensional multidisciplinary couplings handling, multi-fidelity with various input dimensions),




- UQ for multiphysics system analysis and design is a very dynamic field of research and applied in various domains (aerospace, civil engineering, automotive, structure, *etc.*),
- Numerous methods allow now to perform design with uncertainties from modeling to optimization under uncertainties while accounting for multiphysics couplings,
- Several methodological breakthroughs are still locked and need further research (*e.g.* high dimensional multidisciplinary couplings handling, multi-fidelity with various input dimensions),
- Most of current methods still need research to deal with the complexity of real world problems (*e.g.*, scale with the number of uncertain variables, of design variables, of disciplines, of field variables).





Thank you!

For more information \rightarrow





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